

Groundwater regime associated with slope stability in Champlain clay deposits

JEAN LAFLEUR¹ AND GUY LEFEBVRE

Département de Génie Civil, Université de Sherbrooke, Sherbrooke (Qué.), Canada J1K 2R1

Received October 17, 1978

Accepted September 19, 1979

Slope stability analyses in terms of effective stresses are most often based on hypothetical conditions of pore pressure. It is generally assumed that the flow occurs parallel to the slope or even that the conditions are hydrostatic. In fact, *in situ* measurements tend to show that the real situation could significantly deviate from these approximations due to geologic conditions. The influence of various geometric and stratigraphic factors on the groundwater regime and on the stability of slopes was studied with the finite-element method. To illustrate the parametric study, experimental evaluations of the flow patterns are presented at four sites. The stratigraphy and permeability measurements combined with the finite-element method enabled a complete flow net to be drawn and although some hypotheses had to be formulated with regards to the underlying aquifer recharge or permeability anisotropy, reasonable agreement was found between simulated and measured piezometric heads.

La justesse des analyses de stabilité en contraintes effectives des pentes d'argile de la mer Champlain est souvent atténuée par les hypothèses qui sont faites quant à la distribution des pressions interstitielles; ainsi en l'absence de mesures piézométriques, on suppose que l'écoulement se fait parallèlement à la pente ou, de façon plus pessimiste, que les conditions sont hydrostatiques.

En réalité, des mesures *in situ* ont démontré que ces approximations pouvaient s'avérer fausses, et qu'on pouvait relier ces écarts aux conditions géologiques. On a alors entrepris une étude paramétrique à l'aide de la méthode des éléments finis et on a mis en relief l'influence prépondérante sur le régime des eaux souterraines et sur la stabilité des pentes, de couches plus perméables telles que till ou argile fissurée, adjacentes au dépôt d'argile.

En deuxième partie, on présente une étude de quatre cas représentatifs d'écoulement en pente argileuse. La stratigraphie détaillée et les mesures de perméabilité combinées à l'utilisation du programme d'éléments finis ont permis de tracer le réseau d'écoulement complet au voisinage de ces pentes et malgré les hypothèses faites sur la recharge des aquifères sous-jacents à l'argile, ou sur les rapports d'anisotropie de perméabilité, les charges piézométriques calculées concordent bien avec celles qui ont été mesurées.

Can. Geotech. J., 17, 44-53 (1980)

Introduction

Since the early sixties, soil mechanics has progressed significantly in the evaluation of the stability of natural slopes. It is more and more accepted that such slopes should be analysed in terms of effective stresses. Much attention has been devoted to determining the effective strength parameters of the Champlain clay that should be used in the analysis (Lo and Lee 1974; Lefebvre and La Rochelle 1974; Mitchell 1975). The pore-pressure distribution necessary for the analysis is, however, most often based on rather simple assumptions. The flow is frequently assumed to be parallel to the slope or, at worst, the pore pressures are calculated as being under hydrostatic conditions.

Because of geometry and local geology, the flow pattern can differ significantly from the simple models mentioned above. La Rochelle *et al.* (1970) presented

some examples of an important upward gradient existing at the toe of a slope that was at that time related to the configuration of the underlying bedrock. More recently, Hodge and Freeze (1977), after detailing a modelling technique based on the finite element method to describe the groundwater movement on a regional basis, have pointed out the influence of the entire geological environment on the hydraulic conductivity contrasts and anisotropy of the groundwater flow system with an emphasis on the stability of rock slopes.

The purpose of this paper is to show that, due to the geological environment of the Champlain clay, the movement of groundwater in the vicinity of slopes results in a pore-pressure distribution which could be very different from the simple assumptions mentioned above. The first part of the paper illustrates the influence of various factors on the pore-pressure distribution using a modelling technique based on the finite-element method. A parametric slope stability analysis translates the effect of

pressure distribution in terms of the factor of safety against failure. It presents field data obtained at four sites in the Lawrence valley to support the theoretical analysis.

Formation of Clay Deposits

The Champlain clay deposits consist of a relatively thick impermeable layer bounded at its lower and upper portions by pervious layers. At the bottom, there overlies either a till sheet or a fissured granular material at least 100 times as permeable. On top of the clay, upon isostatic unloading, a pattern was developed by the regional alluvial sands were often deposited in sandy layers overlie the clay strata. The upper portion of the clay was desiccated and fissured to a variable extent resulting in all hydraulic conductivity as low as 10⁻¹⁰ cm/s (Lafleur 1978). Another point is with regard to clay deposition: since the rate of sedimentation varied with time, the clay is laminated with sand or silt seams which are equivalent of a permeability anisotropy.

Influence of Various Factors on Pore Pressure Distribution

Modelling Technique

The finite-element method (FEM) is a versatile solution for drawing the flow pattern with different geologic and geometric conditions. The method described in detail by Neuman (1970) easily evaluates the pore pressure at every point in a flow region involving complex geometry and boundary conditions. The position of the phreatic surface is determined by infiltration or evaporation.

The computer program FREESURF (University of Berkeley, California, and based on the Hodge and Freeze (1977) method) was used to solve two-dimensional seepage in an unconfined flow region. The flow region was subdivided into several elements. The input data included the position of each nodal point, hydraulic conductivity in the principal directions, the first and second boundary conditions, the vertical infiltration rate, the boundary conditions. By iterative calculations, the program shifted the position of the phreatic surface until the error between the assumed and the actual position was within acceptable limits. The pressure head computed for each node by the FREESURF were subsequently

¹Present address: Département de Génie Civil, Ecole Polytechnique, Montréal (Qué.), Canada H3C 3A7.

h
sits

é.), Canada JIK 2R1

based on hypothetical parallel to the slope or to show that the real geologic conditions. The water regime and on the substrate the parametric sites. The stratigraphy enabled a complete understanding with regards to the movement was found be-

ntes d'argile de la mer
nt à la distribution des
a suppose que l'écoule-
ue les conditions sont

ons pouvaient s'avérer
n a alors entrepris une
en relief l'influence pré-
sentes, de couches plus

d'écoulement en pente
inées à l'utilisation du
t complet au voisinage
sous-jacents à l'argile,
étriques calculées con-

an important upward gradient of a slope that was at that time. Hodge and Freeze (1977), after using a technique based on the finite element method to describe the groundwater movement on a local basis, have pointed out that the geological environment (by contrasts and anisotropy) of a flow system with an emphasis on rock slopes.

his paper is to show that, due to the movement of the Champlain clay, the groundwater in the vicinity of the pore-pressure distribution is different from the simple assumption. The first part of the paper illustrates the effect of various factors on the pore-pressure distribution using a modelling technique, the finite element method. A parametric study translates the effect of pore-

pressure distribution in terms of the variation of the factor of safety against failure. The second part presents field data obtained at four sites in the St. Lawrence valley to support the theoretical findings.

Formation of Clay Deposits

The Champlain clay deposits can be considered as a relatively thick impermeable stratum always bounded at its lower and upper parts by two more pervious layers. At the bottom, the marine clay overlies either a till sheet or a fissured bedrock or any granular material at least 100 times more permeable. On top of the clay, upon isostatic uplift, a drainage pattern was developed by the regression of the sea as alluvial sands were often deposited. Where no sandy layers overlie the clay stratum, the original upper portion of the clay was desiccated, oxydized, and fissured to a variable extent resulting in an overall hydraulic conductivity as large as 10^{-5} cm/s (Lafleur 1978). Another point is worth consideration with regard to clay deposition: since the conditions of sedimentation varied with time, the clays can be laminated with sand or silt seams that introduce the equivalent of a permeability anisotropy.

Influence of Various Factors on Pore-pressure Distribution

Modelling Technique

The finite-element method (FEM) offered the most versatile solution for drawing the flow nets associated with different geologic and geometric conditions. The method described in detail by Neuman and Witherspoon (1970) easily evaluates the hydraulic head at every point in a flow region involving rather complex geometry and boundary conditions and determines the position of the phreatic surface in conditions of infiltration or evaporation.

The computer program FREESURF developed at Berkeley, California, and based on the Neuman and Witherspoon method (1970) was used to investigate two-dimensional seepage in an unconfined flow region. The flow region was subdivided into 212 quadrilateral elements. The input data consisted of the position of each nodal point, hydraulic conductivities in the principal directions, the first trial position of the phreatic surface, the vertical infiltration rate, and the boundary conditions. By iterative procedure, the heads were calculated at each nodal point and the program shifted the position of the phreatic surface until the error between the assumed and the calculated position was within acceptable limits. The total head and the pressure head computed for each nodal point by FREESURF were subsequently processed by

another program so that equipotential and equipressure lines could be drawn by a tracing table.

Factors and Assumptions Considered in the Analysis

The parametric study was undertaken to evaluate the relative influence of different factors on the flow regime associated with slopes and 22 models were finally considered in the analysis. The following factors were varied in accordance with the physical context of the Champlain Sea area: infiltration rate, vertical position of the lower aquifer with respect to the toe of the slope; permeability anisotropy; and geometry (extent and shape) of the drainage basin.

The definitions and symbols are given in Fig. 1. Some general assumptions were made with regard to boundary conditions, slope dimensions, and permeability distribution: the calculations were made for two-dimensional cases with uniform hydraulic conductivity in each zone; even though the lower aquifer can in fact be more permeable than the clay, by several orders of magnitude, the hydraulic conductivity ratio was assumed to be less than 100. The profile corresponds to a typical stable Champlain clay slope: angle, 18° ; thickness of the upper permeable clay crust, 2 m; and height, 15 m. Finally, the upstream and downstream boundaries corresponding respectively to the water divide and thalweg line were implicitly impervious boundaries since they constituted with the bottom line the extreme flow line of this closed system; on the other hand, if the adjacent drainage basins are symmetrical, these boundaries are vertical as assumed in this parametric study.

Existence and Influence of a Superficial Layer

Since a permeable layer was found to be invariably present at the top of the clay deposits, the infiltration capacity of the soil was presumed to be influenced by its permeability or by the rates of infiltration. The position of the water table and the flow net in this layer were studied and it was found that when the infiltration rate was taken equal to the average annual precipitation rate, the water table was brought to the ground surface (implying runoff) and flow occurred parallel to the slope; on the other hand, with a much lower rate (100 times less) the phreatic surface was lowered, but flow still occurred parallel to the slope in the upper aquifer. Although these results did not take into account the effect of evapo-transpiration on infiltration rates and decreasing hydraulic conductivity with depth in the upper aquifer, they pointed out firstly that the assumption of water level at the ground surface during periods of high infiltration can be justified, and for this reason the other factor were studied assuming no upper aquifer and water

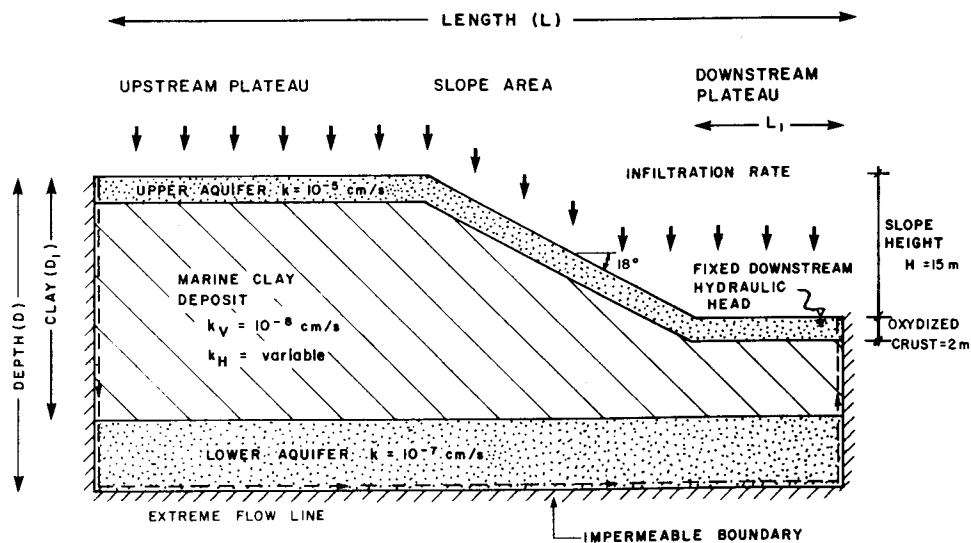


FIG. 1. Parametric study: definition of variables and assumptions.

level at the ground surface for simplicity of calculation. Secondly, it was shown that the upper aquifer can result in flow parallel to the slope, a justifiable assumption when analysing shallow landslides in superficial clay.

Influence of a Lower Aquifer

In relation to deep failures, the parametric study of the groundwater regime surrounding slopes shows that the lower aquifer has a maximal influence on the distribution of pore pressures in the intact clay, and that this distribution can be altered significantly from the so-called hydrostatic conditions. The resulting flow nets are shown in Fig. 2 for different positions of the lower aquifer. The intensity of the upward gradients in the lower part of the slope can be related directly to the closeness of the equipotentials; these results are presented differently in Fig. 3 where the vertical gradients on three axes have been plotted as a function of the position of the aquifer. The upward gradients at the toe of the slope, which are of interest for stability computations, show different patterns if the lower limit of the clay layer is below or above the toe level: above, the entire deposit is underdrained, but below, the clay is submitted to artesian pressure and the upward gradient can be greatly in excess of the critical value of 0.6 (assuming a soil weighing 16 kN/m^3 , this implies that the effective stress is zero and that the shear strength is reduced to its cohesion component).

Influence of Permeability Anisotropy

In Fig. 4 the absolute value of the gradients is seen

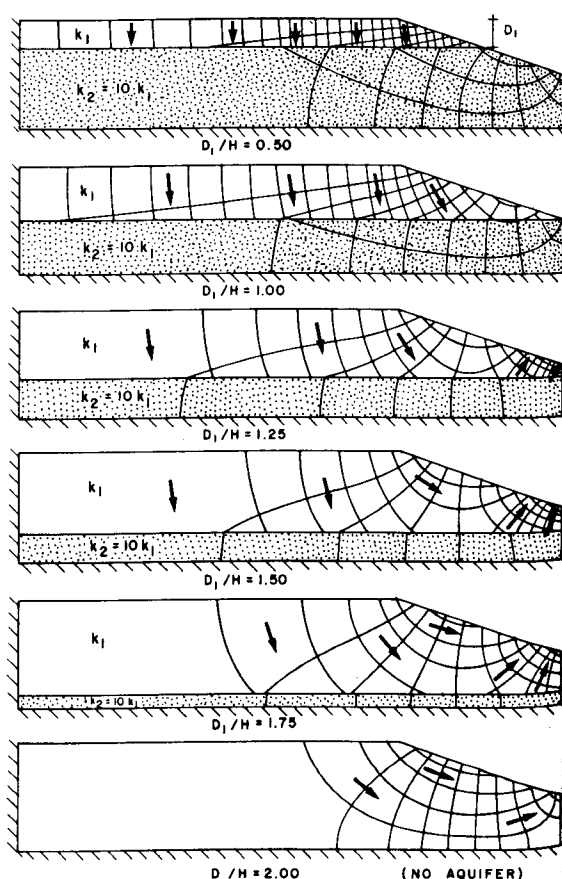


FIG. 2. Flow nets: influence of position of lower aquifer.

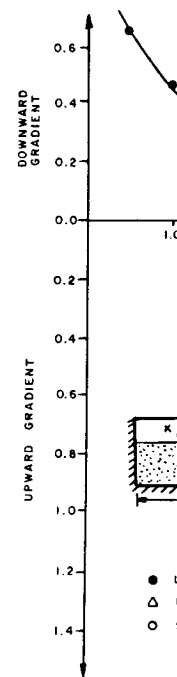


FIG. 3.

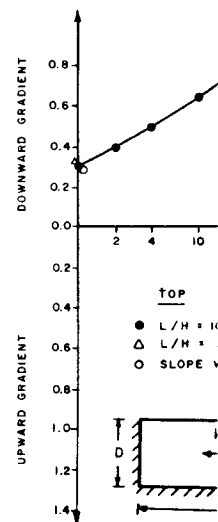
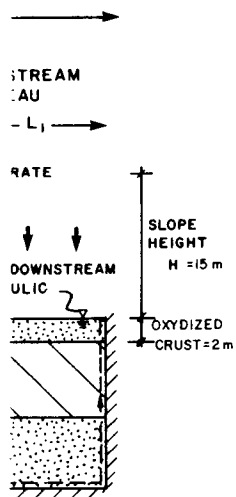


FIG. 4.

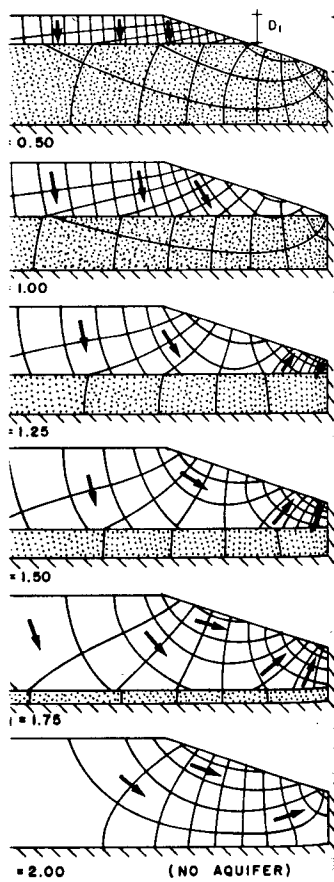
to increase approximately with anisotropy ratio (r_k) up to a

Influence of Geometry

The influence of geometry on the flow nets is shown in Fig. 3 for the slope with a fixed downstream hydraulic head. Fig. 4 for the anisotropic clay: the presence of a downstream hydraulic head has a perceptible influence on the distribution of the top and midheight of the



BOUNDARY
conditions.



Influence of position of lower aquifer

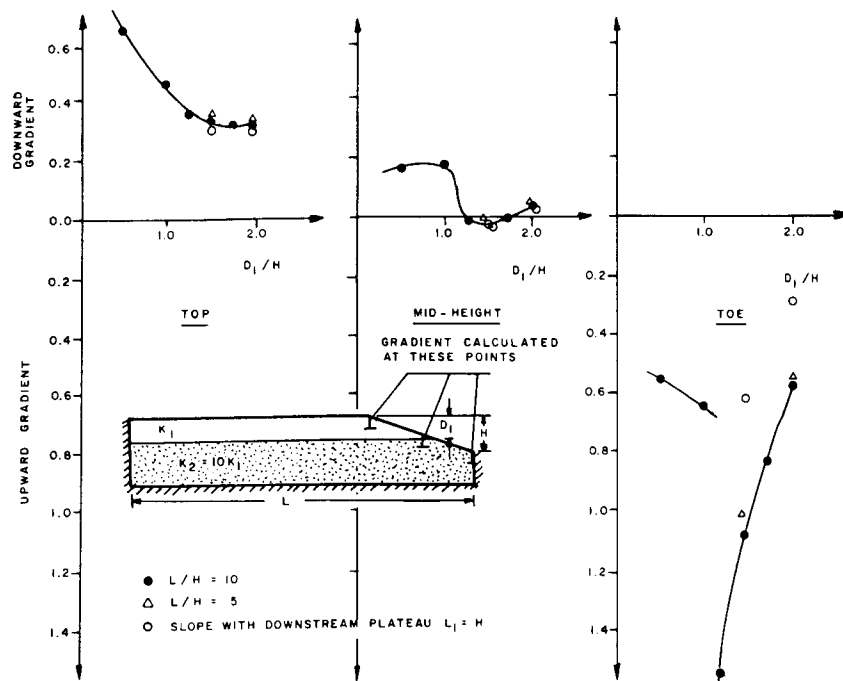


FIG. 3. Influence of the position of lower aquifer on hydraulic gradient.

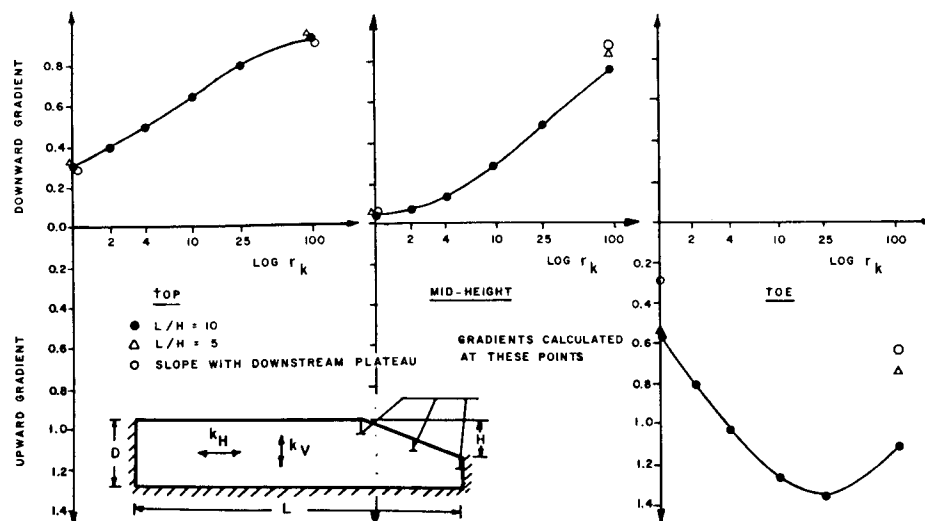


FIG. 4. Influence of anisotropy ($r_k = k_H/k_V$) on hydraulic gradients.

to increase approximately with the logarithm of the anisotropy ratio (r_k) up to a ratio of 25.

Influence of Geometry

The influence of geometry can readily be observed in Fig. 3 for the slope with a lower aquifer and in Fig. 4 for the anisotropic clay: the length of the basin and the presence of a downstream plateau have no perceptible influence on the downward gradients at the top and midheight of the slope. On the other

hand, both factors can decrease the upward gradient at the toe of the slope by 50% provided that the length of the downstream plateau $L_1 \geq H$, and the length of the basin $L \leq 5H$, where H is the slope height.

Significance of Pore-Pressure Distribution in Slope Stability Analysis

To assess the degree of influence of these factors stability analyses were performed for a typical slope

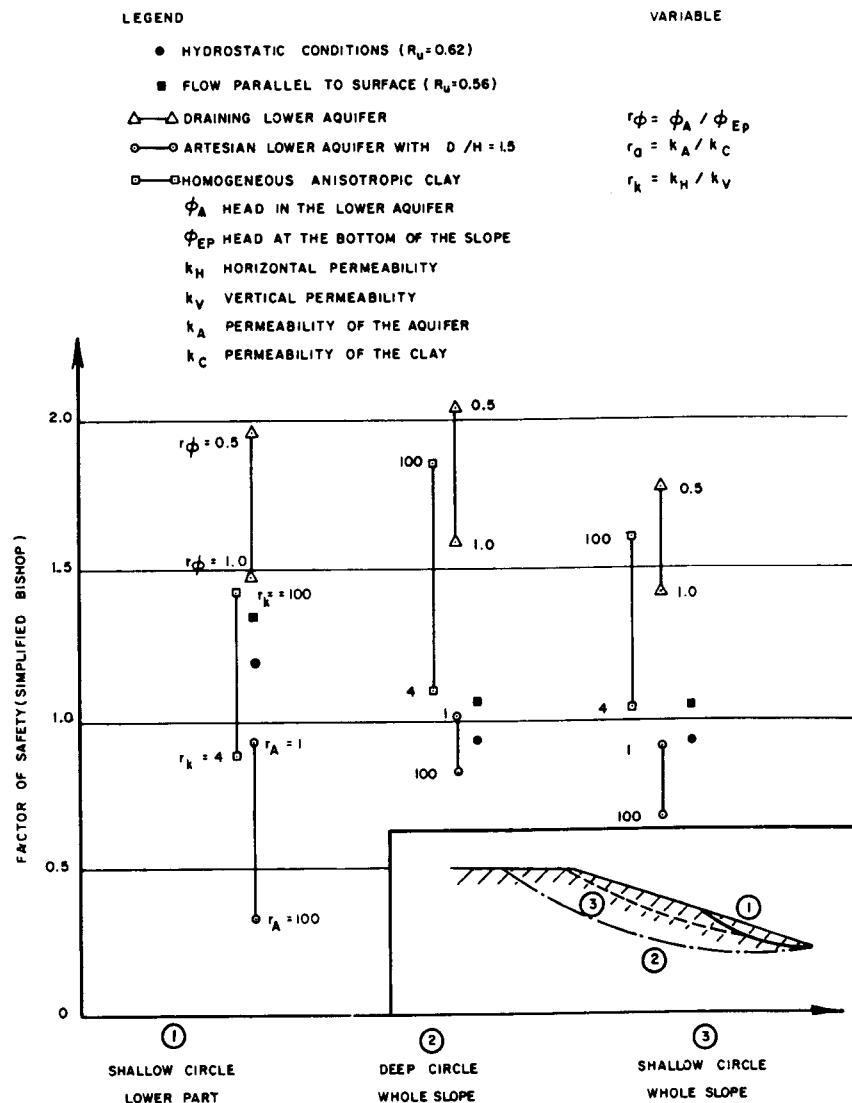
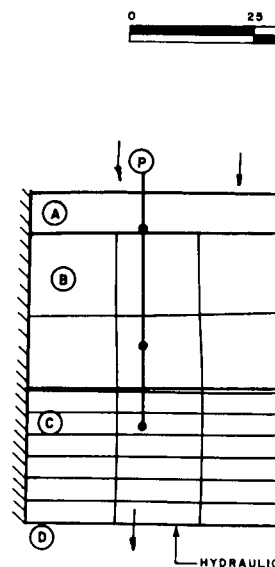


FIG. 5. Influence of groundwater regime on factor of safety.

having the following characteristics: $c' = 7$ kPa; $\phi' = 31^\circ$; $\gamma = 16$ kN/m³; phreatic surface at ground level; and no tension cracks. The stability analyses were done by the simplified Bishop method using a computer program in which the positions of equipressure lines could be entered directly. Three specified slip circles were chosen according to various possible locations of failure surface: ① shallow circle involving the toe of the slope; ② deep circle involving the whole slope; and ③ shallow circle involving the whole slope.

The results are shown in Fig. 5 for these three circles; the different groundwater conditions caused the factor of safety to vary between 0.3 and 2.0. This

scatter for a unique slope with varying groundwater conditions is related to whether the lower aquifer is drained or artesian: a drained aquifer with $\phi_A/\phi_{EP} = 0.5$ gives a factor of safety of 2. If this same aquifer is artesian and the ratio of the coefficient of permeability of the aquifer to that of the clay is 100, the factor of safety is shown to vary between 0.3 and 0.5. Finally, the overall effect of assuming permeability anisotropy is a general increase in the factor of safety with respect to the isotropic medium. The values obtained with the usual assumptions for pore water pressure distributions (hydrostatic conditions or flow parallel to surface) are close to unity.



Comparison with Observed

The four sites have been selected to provide a wide variation of conditions. They are underdrained at two sites: at St. Ambroise, which is thicker and drained to an artesian aquifer below the toe of the slope. The Nicolet sites involve clay deposits with different geometries and permeabilities. The deposit is large in extent compared to the St. Ambroise, which involves a small deposit between rock valley walls. The sites have been investigated at St. Urbain and St. Ambroise. The fieldwork generally consisted of a stratigraphic investigation with the use of piezometer tips on vertical faces of exposed faces of the slope. Permeability tests in auger-holes were also performed. Measurements of hydraulic conductivity were obtained at the Nicolet sites. A piezometer was developed to register possible fluctuations in the position of the water table during springtime. Finally, the overall effect of assuming permeability anisotropy, permeability evaluation, and boundary conditions were compared with the present analysis to draw a flow pattern. Our knowledge of the permeability of the boundary condition was not in complete agreement was observed.

TABLE

 ϕ_A / ϕ_{EP}
 A / k_C
 H / k_V

0.5

1.0



③
LOW CIRCLE
PIEZO SLOPE

fety.

slope with varying groundwater to whether the lower aquifer is a drained aquifer with ϕ_A / ϕ_{EP} safety of 2. If this same aquifer of the coefficient of permeability of the clay is 100, the factor to vary between 0.3 and 0.5 effect of assuming permeability increase in the factor of safety isotropic medium. The values of usual assumptions for porous (hydrostatic conditions or flow are close to unity.

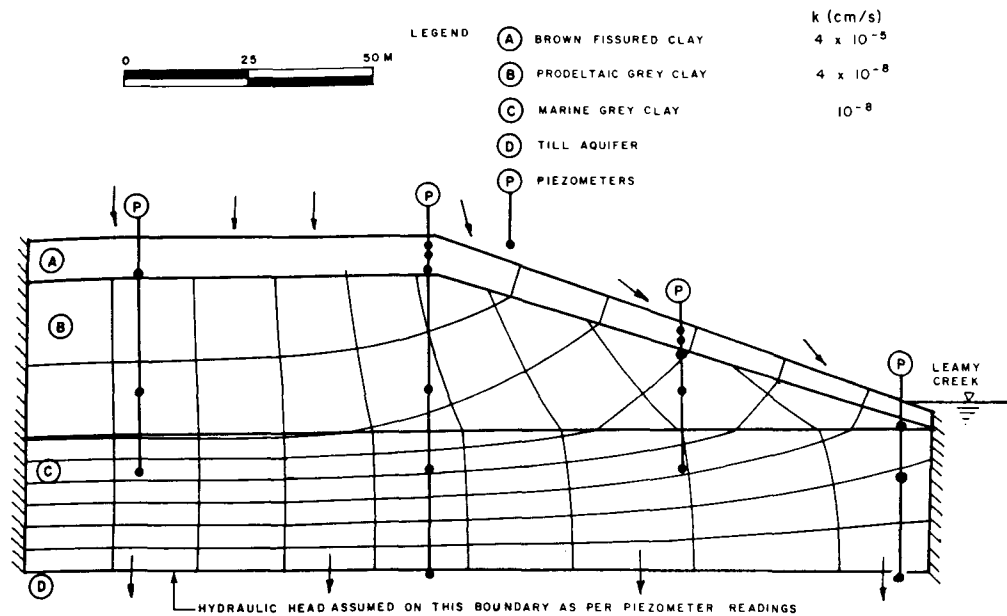


FIG. 6. Flow net: Hull.

Comparison with Observed Flow Patterns

The four sites have been selected to represent a wide variation of conditions. The clay deposits are underdrained at two sites: at St-Urbain the clay is drained above the toe of the slope, whereas at Hull it is thicker and drained to an aquifer lying much below the toe of the slope. The St-Ambroise and Nicolet sites involve clay deposits fed by artesian aquifers with different geometries. The Nicolet clay deposit is large in extent compared with that at St-Ambroise, which involves a narrow clay tongue lying between rock valley walls. Anisotropy effects have been investigated at St-Urbain.

The fieldwork generally consisted of a detailed stratigraphic investigation with tube sampling, visual inspection of exposed faces of the deposits, installation of piezometer tips on vertical axes near the slope, and permeability tests in auger-holes and open-tube piezometers. Measurements of hydraulic heads in the slope area were obtained at time intervals close enough to register possible fluctuations. A special surface piezometer was developed to record the maximum position of the water table in the upper clay crust during springtime. Finally, the stratigraphy, piezometry, permeability evaluation, and measured boundary conditions were combined in a finite element analysis to draw a flow net at each site. Where our knowledge of the permeability coefficients and of the boundary conditions was accurate, a reasonable agreement was observed between meas-

ured and calculated piezometric heads. However, at St-Urbain and Nicolet some assumptions or adjustments had to be made with regard to the permeability anisotropy ratio and boundary conditions, so that both pressure distributions would become equal.

Site No. 1—Hull

This site is located in the Leamy Creek valley in the north end of the city. The valley is symmetrical and the plateau is fairly horizontal. The idealized geometry, the location of piezometers, and the stratigraphy are given in Fig. 6. The sedimentary deposit consists of the following four zones.

A. *Brown fissured and oxydized clay crust*: Highly fractured and containing roots for the first 2–3 m. Overall *in situ* permeability measurements by different methods gave a value of $k = 2\text{--}30 \times 10^{-5}$ cm/s.

B. *Grey silty clay*: This material is believed to correspond to the prodeltaic clay described by Fransham and Gadd (1977). Permeability measured in open porous stone piezometers was $k = 4 \times 10^{-6}$ cm/s.

C. *Grey silty marine clay*: Some traces of organic matter appeared in this horizon. Piezometric measurements indicate that this clay is slightly less permeable than the one above and a value of 10^{-8} cm/s was assumed for this stratum.

D. *Till*: This aquifer has been identified as a silty sand and gravel and, being drained towards the Gatineau River flowing 1 km east of the site at a

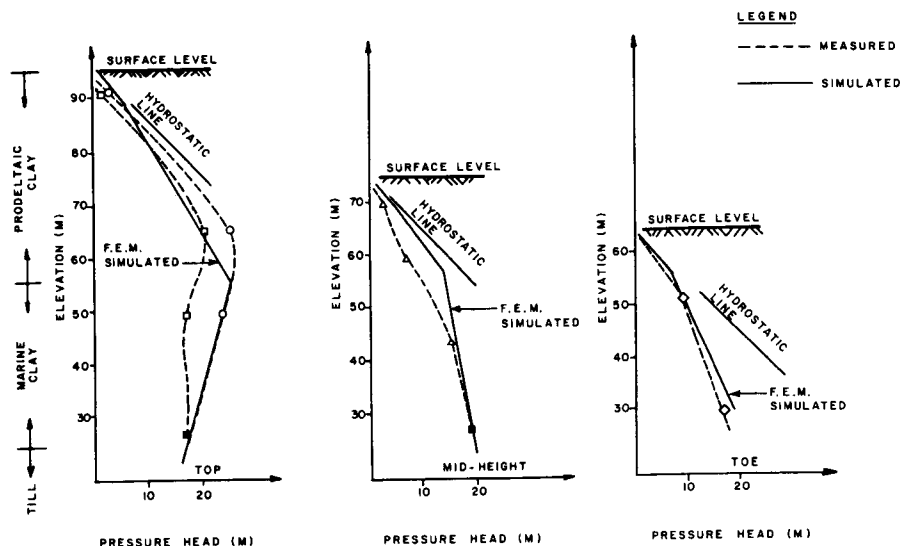


FIG. 7. Piezometric heads: Hull.

lower elevation, this stratum is responsible for the general downward gradient measured on this site. Similar findings have also been reported by Jarret and Eden (1970) for a site east of the City of Ottawa.

The flow net shown in Fig. 6 displays the generalized downward flow resulting from the small hydraulic head assumed and measured at two points in aquifer D. Piezometric measurements were made with Glötzl cells at different depths along four vertical axes; the comparison between the measured and the simulated distribution of pore pressures is shown in Fig. 7. In the superficial layer, the large permeability given to the crust created a flow parallel to the slope and the recording piezometers indicated that the water table fluctuated rather rapidly (1 m/week) and could approach the ground surface in every part of the slope.

Site No. 2—St-Urbain

This site is located along the Rivière-du-Gouffre, 100 km east of Quebec City, and this clay terrace, remnant of the Champlain Sea episode, lies along the sides of a narrow valley in the Precambrian Shield. Conditions are given in Fig. 8. The following three types of material have been identified.

A. Grey silty marine clay: Contains very thin discontinuous sand seams and traces of organic matter.

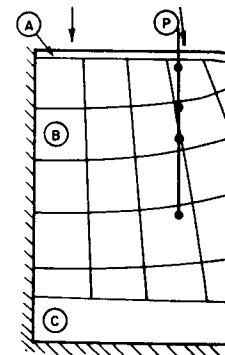
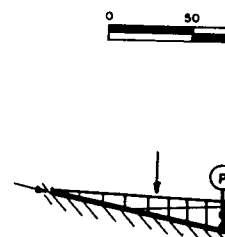
B. Stratified clay and sand: Below a certain level, deposit B consists of sand layers gradually thickening with depth. An important water seepage surface could be observed all year round along the river bank at that level.

C. Till or fractured rock aquifer: Ablation till covering the hillside is believed to extend under the marine clay deposit but if not so, the fractured bedrock constitutes an equivalent aquifer.

The resulting flow net is given in Fig. 8. Because no information on *in situ* permeability was available, especially with regard to anisotropy, assumptions had to be made so that the resulting flow net would conform with piezometer readings. Firstly, an absolute value of horizontal permeability and an anisotropy ratio $k_H/k_V = 100$ were assigned on the basis of grain size and the spacing of layers, and this large ratio was found to introduce a second phreatic surface at the interface of layers A and B. Because this was contradictory to the observation of steady seepage on the river bank face, a ratio of 10 was finally assumed so that calculated heads would conform with those measured at two vertical axes. At this site, Glötzl cells combined with open-tube piezometers indicated a strong downward gradient in the upper clay A, whereas the three piezometric tips in soil B gave a distribution approaching hydrostatic conditions.

Site No. 3—St-Ambroise

This site is contained in a narrow valley located approximately 70 km northeast of Montreal and is bounded by bedrock slopes. In the middle of the 40 m clay deposit, a small river has cut a channel 20 m deep, the banks of which have been flattened by past landslides in the exceptionally sensitive clay. Typically, three types of soils have been identified

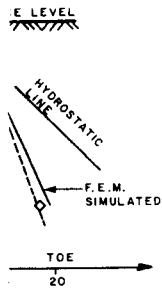


A. Desiccated clay crust: Although thinner than at Hull, hydraulic conductivity of $k = 1-6 \times 10^{-4}$ cm/s was measured in this 2 m layer.

B. Grey silty marine clay: This layer is homogeneous down to the 20 m depth. Very thin sand seams have been identified. Conductivities were measured at two points and were found to vary between 1 and 10 cm/s.

C. Till: This layer has been identified by auger-boring as gravelly and sandy. These conditions and piezometric data are summarized in Fig. 9 where the piezometric data are given. Piezometric measurements were taken with open porous stone

LEGEND
 - - - - - MEASURED
 ——— SIMULATED



URE HEAD (M)

ed rock aquifer: Ablation till covers is believed to extend under the but if not so, the fractured bed equivalent aquifer. Flow net is given in Fig. 8. Because *in situ* permeability was available and to anisotropy, assumption that the resulting flow net would meter readings. Firstly, an absolute horizontal permeability and an anisotropy = 100 were assigned on the basis of spacing of layers, and this large introduce a second phreatic surface of layers A and B. Because of the observation of steady seepage on the bank face, a ratio of 10 was finally calculated heads would conform at two vertical axes. At the combined with open-tube piezometers along downward gradient in the toe as the three piezometric tips distribution approaching hydrostatic

No. 3—St-Ambroise

located in a narrow valley located 15 km northeast of Montreal on the steep slopes. In the middle of the valley a small river has cut a channel, the exception of which have been flattened. The exceptionally sensitive clay layers of soils have been identified

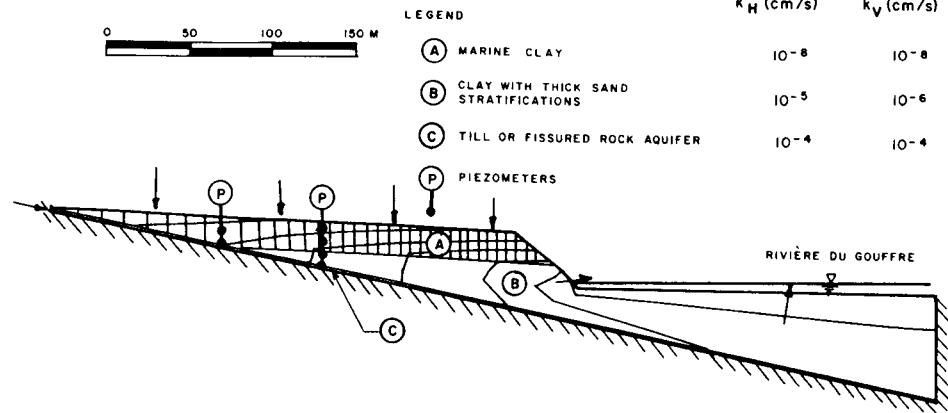


FIG. 8. Flow net: Saint-Urbain.

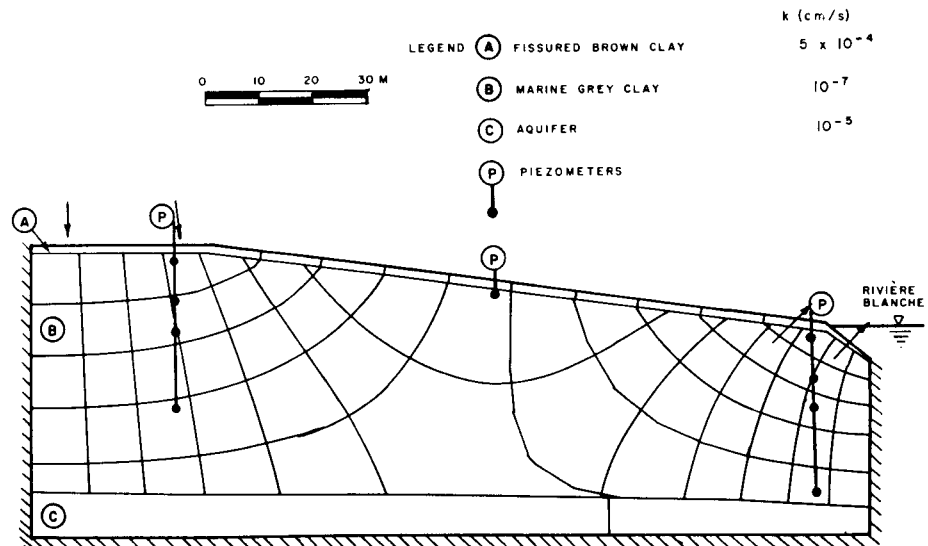


FIG. 9. Flow net: Saint-Ambroise.

A. Desiccated clay crust: Although the crust is less thick than at Hull, hydraulic conductivities of the order of $k = 1-6 \times 10^{-4}$ cm/s have been measured in this 2 m layer.

B. Grey silty marine clay: This clay is relatively homogeneous down to the 20 m depth and afterwards very thin sand seams have been observed. Hydraulic conductivities were measured through porous tips and were found to vary between $k = 1$ and 4×10^{-5} cm/s.

C. Till: This layer has been identified indirectly by auger-boring as gravelly and sandy material.

These conditions and piezometer locations are summarized in Fig. 9 where the resulting flow net is given. Piezometric measurements have all been taken with open porous stone piezometers driven

along two vertical axes at 9, 18, and 30 m depth. At the toe of the slope, where artesian conditions prevailed, manometers were fitted to register the positive pressures. Groundwater levels were measured at the 4 m depth by self-recording piezometers. Figure 1 gives the comparison between simulated and measured pore-pressure distributions. The results show relatively small gradients, perhaps related to the geometry of the slope, and the impermeable boundary conditions inferred, which tend to confirm the noninfluence of recharge of the lower aquifer by the adjoining valley walls. On the other hand, measurements support the idea that the water table comes near the surface during periods of high infiltration and lowers to the level of the intact grey clay during the dry summer spells.

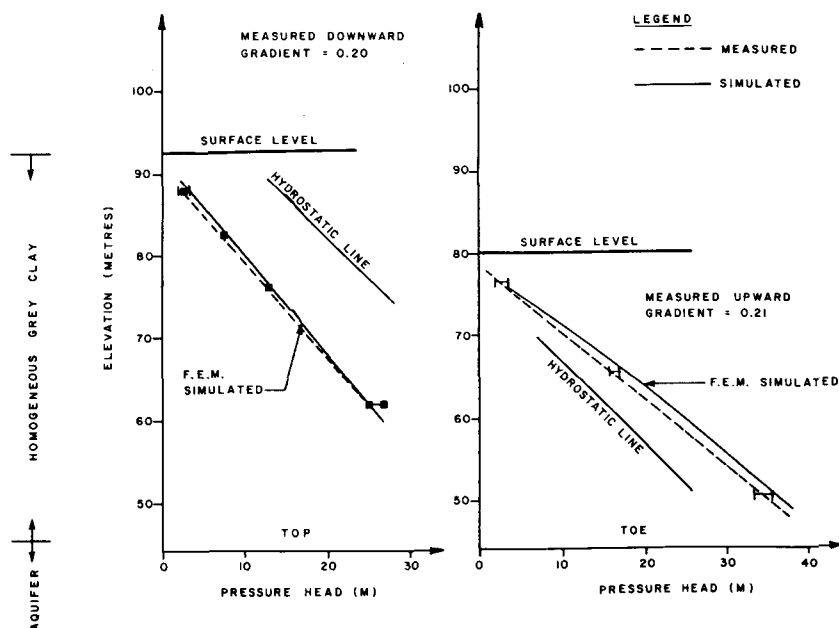


FIG. 10. Piezometric heads: St-Ambroise de Kildare.

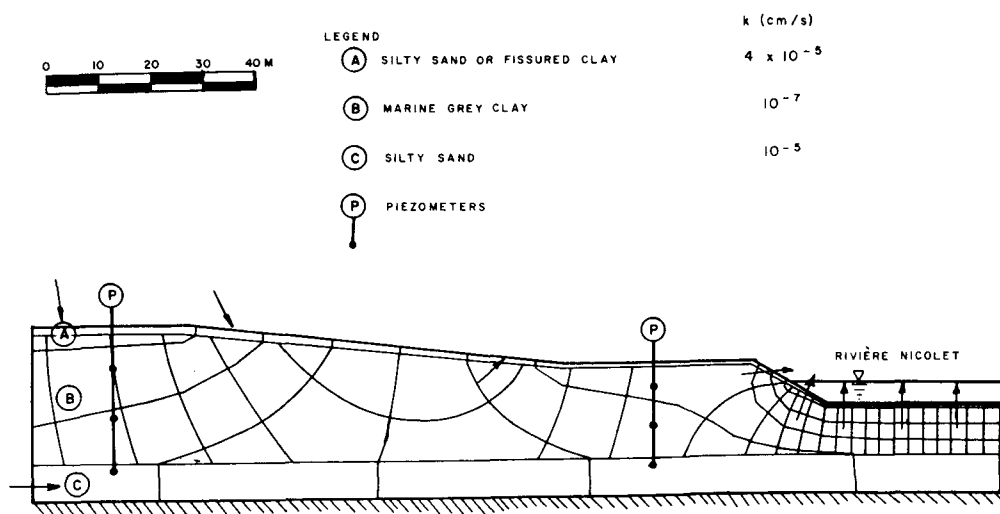


FIG. 11. Flow net: Nicolet.

Site No. 4—Nicolet

This site is located near the shore of Lac St-Pierre on a relatively level clay plateau cut only by the Nicolet river, creating an 18 m gentle slope except for the immediate river bank. The geometry and ground conditions are given in Fig. 11 and the stratigraphy can be described as follows.

A. *Compact silty sand*: Hydraulic conductivity assumed to be $k = 4 \times 10^{-5}$ cm/s.

B. *Grey silty clay*: Hydraulic conductivity assumed to be 10^{-7} cm/s.

C. *Sandy and silty gravel*: Hydraulic conductivity assumed to be 10^{-5} cm/s. Although not confirmed, the continuity of this deposit throughout the section has been assumed.

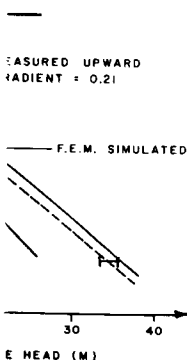
The main feature of the flow net shown in Fig. 11 is the large upward gradient that can be anticipated under the river, provided the C layer exists in this location. Piezometers were of the Glözl type because of the great extent of the deposit, a small downward gradient at the top of the slope had to be assumed to conform with the piezometric readings at that location.

Discussion

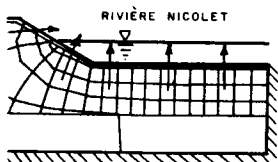
With some limitations with regard to the distribution of piezometer tips, the use of these tips, and the hydraulic conductivity measurements, the present paper confirms the assumptions with regard to groundwater flow in a superficial permeable layer (water table near the surface) and points out the influence of regional geology on pore-pressure distribution in the vicinity of slopes made up of non-homogeneous layers. The position of the low water level in the Champlain Sea at the toe of the slope appears to control the upward hydraulic gradient which directly influence the magnitude of the effective stresses normal to the failure surface and influence the shear strength of the soils. If the upward gradients exceed the vertical effective stresses, the shear strength decreases. On one hand, if the aquifer is confined and located below the slope, the magnitude of the upward gradient is inversely proportional to the vertical effective stress between the toe of the slope and the water table and can substantially exceed the vertical effective stress. On the other hand, if the aquifer is unconfined, a small hydraulic head, the clay deformation leads to a generalized downward gradient which increases the effective stresses and increases the shear strength.

Permeability anisotropy is acknowledged as a puzzling factor, because it could not be determined *in situ* by direct measurement and the present study has shown its considerable influence on the flow regime. The absolute value of the hydraulic conductivity varies exponentially with the anisotropy ratio to a value of 25. The site at Nicolet is a stratified soil and the lack of a clear-cut result for r_k precludes clear-cut results for r_k . With regard to the marine deposits at the investigated sites, visual inspection does not support the assumption of permeability anisotropy.

Legend
 - - - - - MEASURED
 ——— SIMULATED



c.
 k (cm/s)
 4×10^{-5}
 10^{-7}
 10^{-5}



gravel: Hydraulic conductivity of 1 cm/s. Although not confirmed, it is assumed that the gravel deposit throughout the section.

of the flow net shown in Fig. 1, the gradient that can be anticipated is provided the C layer exists in the deposits were of the Glötzl type and to a certain extent of the deposit, a small gradient at the top of the slope had to be compared with the piezometric reading.

Discussion

With some limitations with regard to the spatial distribution of piezometer tips, the time of response of these tips, and the hydraulic conductivity measurements, the present paper confirms the usual assumptions with regard to groundwater behaviour in the superficial permeable layer (water level at surface in period of high infiltration rate and flow parallel to the surface) and points out the great influence of regional geology on pore-pressure distribution in the vicinity of slopes made up of massive marine clay layers. The position of the lower aquifer (always present in the Champlain Sea context) related to the toe of the slope appears to control the magnitude of the upward hydraulic gradients. These gradients directly influence the magnitude of the effective stresses normal to the failure surface and therefore influence the shear strength of these low-cohesion soils. If the upward gradients exceed the critical value, the vertical effective stresses become nearly zero, as does the shear strength. On one hand, if the lower aquifer is confined and located below the toe of the slope, the magnitude of the upward gradients is inversely proportional to the vertical distance between the toe of the slope and the top of the aquifer and can substantially exceed the critical gradients. On the other hand, if the aquifer is drained and has a small hydraulic head, the clay deposit is submitted to a generalized downward gradient, which implies an increase in effective stresses and consequently an increase in shear strength.

Permeability anisotropy is acknowledged to be a puzzling factor, because it could not be determined *in situ* by direct measurement and the finite-element study has shown its considerable influence on the flow regime. The absolute value of the gradients varies exponentially with the anisotropy ratio r_k up to a value of 25. The site at St-Urbain involved stratified soil and the lack of piezometers in this stratum precludes clear-cut results in the value to be set for r_k . With regard to the marine clay deposits of the investigated sites, visual inspection of the samples does not support the assumption of permeability anisotropy.

Conclusion

The aim of this study has been a better comprehension of the groundwater phenomena associated with the stability of natural slopes consisting primarily of soft sensitive Champlain Sea clays. It provides insight through a factor that is often subjective or indeterminate in stability analysis of these slopes in terms of effective stresses, namely, the pore-pressure distribution on the failure surface. It has been shown that with reasonable knowledge of the stratigraphy and of the boundary conditions (subdrainage or recharge by sloping bedrock) it is possible to draw a complete flow net from which the pore pressures can be adequately determined.

Acknowledgment

This research was financed by the Québec Ministry of Natural Resources and conducted at the Université de Sherbrooke.

- FRANSHAM, P. B., and GADD, N. R. 1977. Geological and geomorphological controls of landslides in Ottawa Valley, Ontario. *Canadian Geotechnical Journal*, 14, pp. 531-539.
- HODGE, R. A. L., and FREEZE, R. A. 1977. Groundwater flow systems and slope stability. *Canadian Geotechnical Journal*, 14, pp. 466-476.
- JARRETT, P. M., and EDEN, W. J. 1970. Groundwater flow in eastern Canada. *Canadian Geotechnical Journal*, 7, pp. 326-333.
- LAFLEUR, J. 1978. Influence de l'eau sur la stabilité des pentes naturelles d'argile. Thèse Ph.D., Département de Génie Civil, Université de Sherbrooke, Sherbrooke (Qué.).
- LA ROCHELLE, P., CHAGNON, J. Y., and LEFEBVRE, G. 1970. Regional geology and landslides in the marine clay deposits of eastern Canada. *Canadian Geotechnical Journal*, 7, pp. 145-156.
- LEFEBVRE, G., and LA ROCHELLE, P. 1974. The analysis of two slope failures in cemented Champlain clays. *Canadian Geotechnical Journal*, 11, pp. 89-108.
- LO, K. Y., and LEE, C. F. 1974. An evaluation of the stability of natural slopes in plastic Champlain clays. *Canadian Geotechnical Journal*, 11, pp. 165-181.
- MITCHELL, R. J. 1975. Strength parameters for permanent slopes in Champlain Sea clays. *Canadian Geotechnical Journal*, 12, pp. 447-455.
- NEUMAN, S. P., and WITHERSPOON, P. A. 1970. Finite element method of analysing steady seepage with a free surface. *Water Resources Research*, 6(3), pp. 889-897.